

# THE ALPHA FIELD CASE STUDY

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TPG4140 NATURGASS

November 10, 2010

- Deliverability and performances
- The Alpha gas field data
- Material balance and z-factor
- PSS flow equation for gas
- Pressure function (pseudopressure) and viscosity
- The Alpha gas pressure function (polynomial fit)
- The Alpha gas well data
- Pressure drop in gas wells
- Inflow performance and outflow performance
- Summary

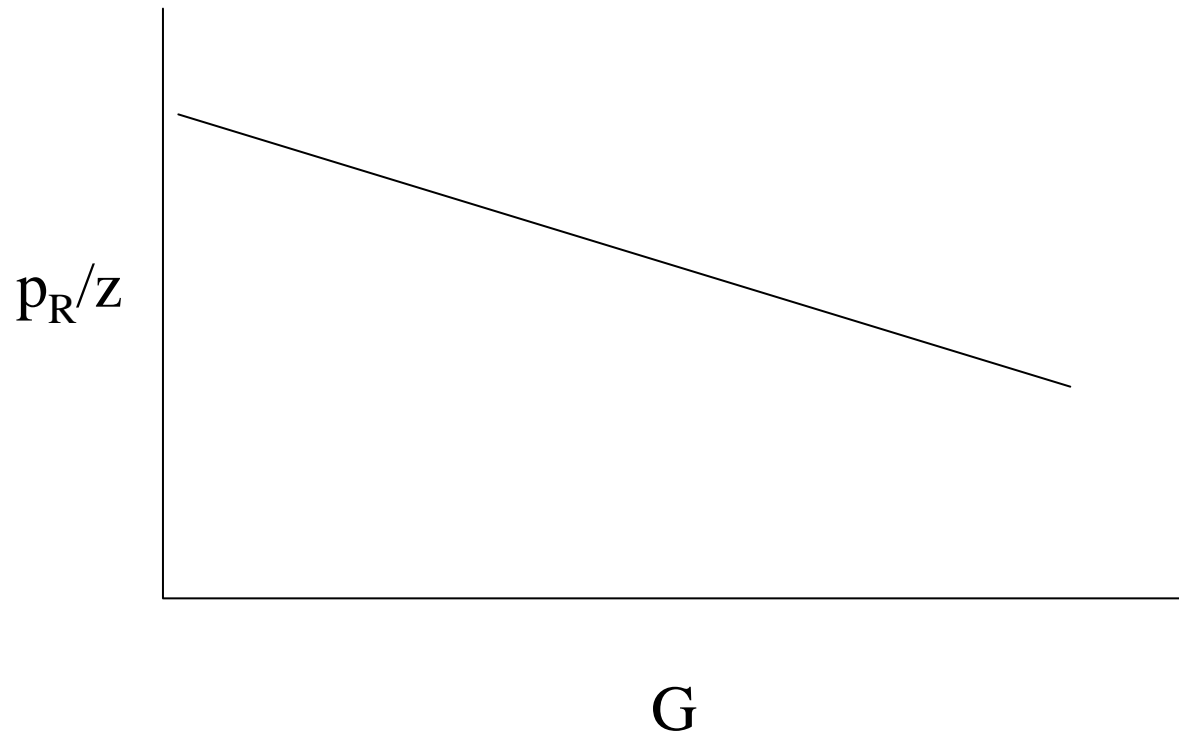
# **Deliverability and Performances**

## Analyse and Synthesis

- Pressure profile from reservoir to wellhead is analysed in terms of several performances.
- Reservoir performance gives reservoir pressure with time, which is used in inflow performance plot.
- Shape of inflow performance plot remains the same with time, unless near-wellbore damage occurs due to production.
- Tubing performance curve plotted together with inflow performance, gives the well production rate where the two curves cross each other.

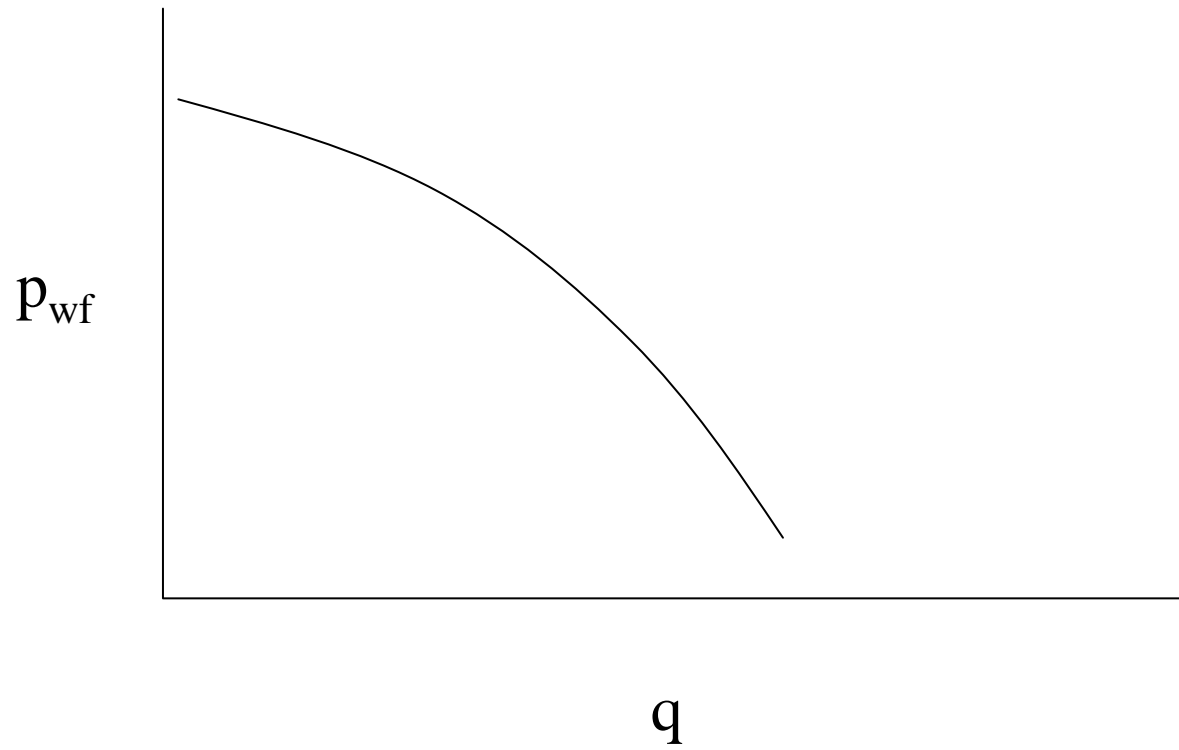
# Deliverability and Performances

## Reservoir Performance



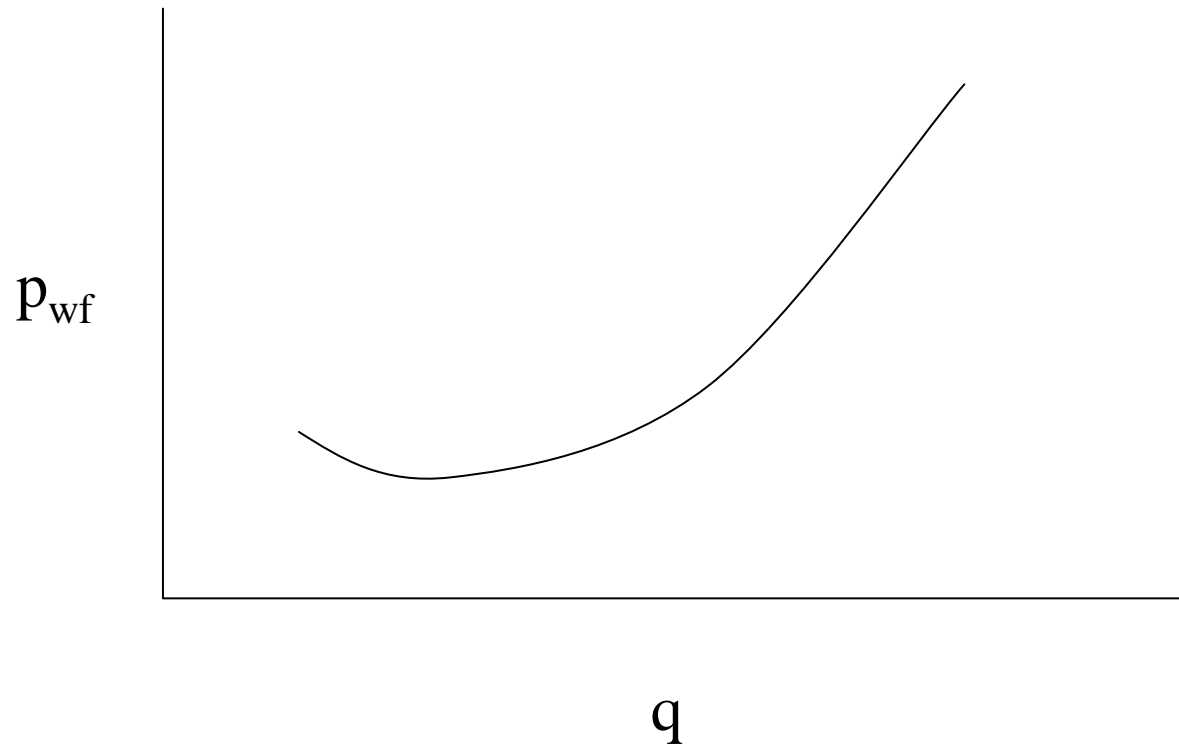
# Deliverability and Performances

## Inflow Performance

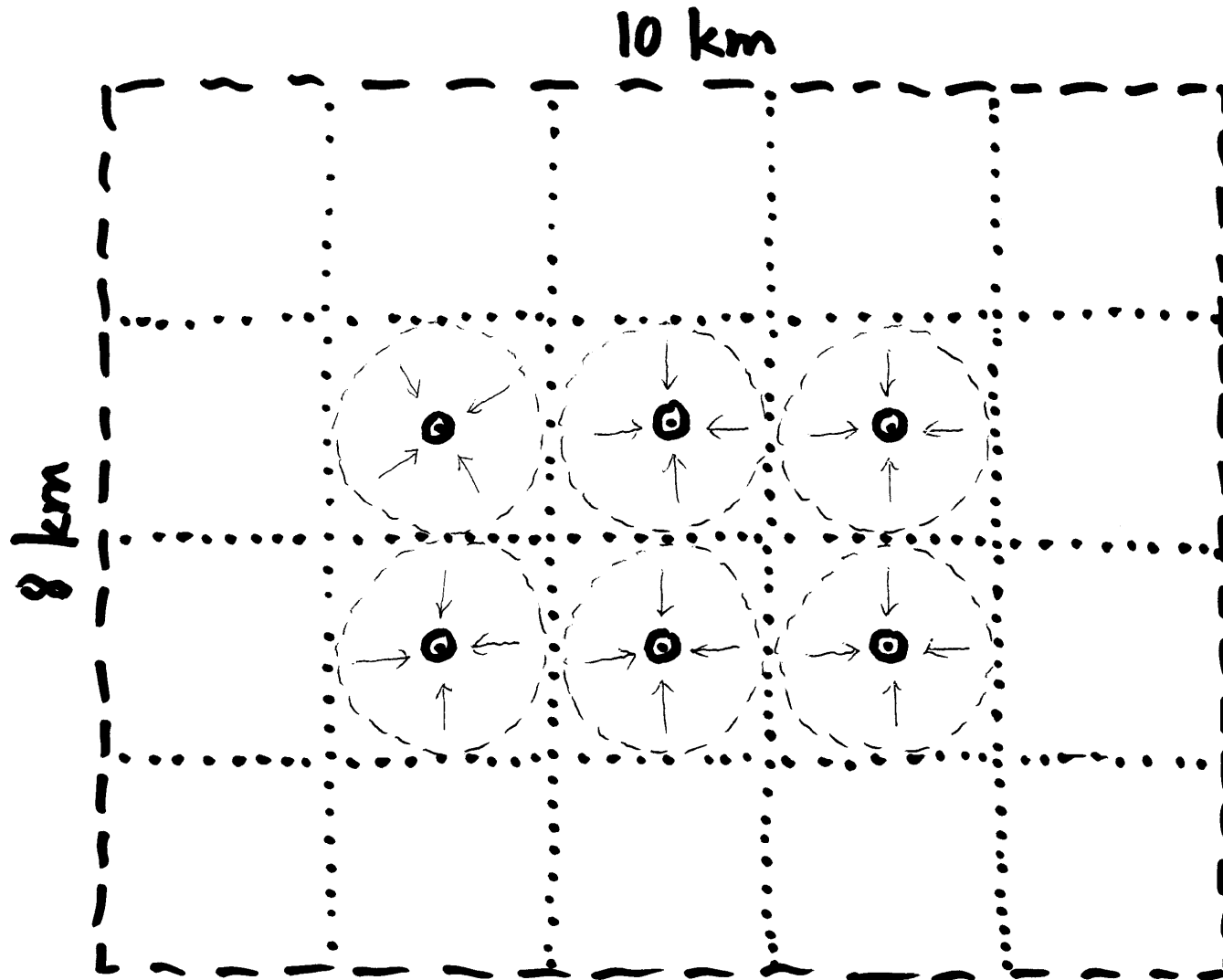


# Deliverability and Performances

## Tubing Performance



# The Alpha Gas Field



| <b>Field data</b>                        |           |                 |
|--|-----------|-----------------|
| Areal og reservoir, AR                   | 80        | km <sup>2</sup> |
| Thickness, hR                            | 25        | m               |
| Average reservoir pressure, pR           | 285       | bara            |
| Average reservoir temperature, TR        | 88        | °C              |
| Water depth, dW                          | 800       | m               |
| Reservoir depth, dR                      | 2600-2650 | TVD MS L        |
| Average permeability, k                  | 200       | md              |
| Porosity, $\phi$                         | 25,00 %   |                 |
| Water Saturation, S w                    | 20,00 %   |                 |
| Recovery factor, RF                      | 60,00 %   |                 |
| Z- factor                                | 0,9334    |                 |
| Specific gravity                         | 0,60      |                 |
| Molecular weight of gas (from hysys), Mg | 17,45     |                 |
| Gas viscosity, $\mu$                     | 1,92E -02 | cp              |
| Drainage radius each well                | 1000      | m               |

# Material Balance for Natural Gas Fields

## Volumetric Balance

Gas volumes taken at standard conditions (s.c.)

Constant volume reservoir without water influx

$G_i$  = Gas initially in place (resource, not reserve)

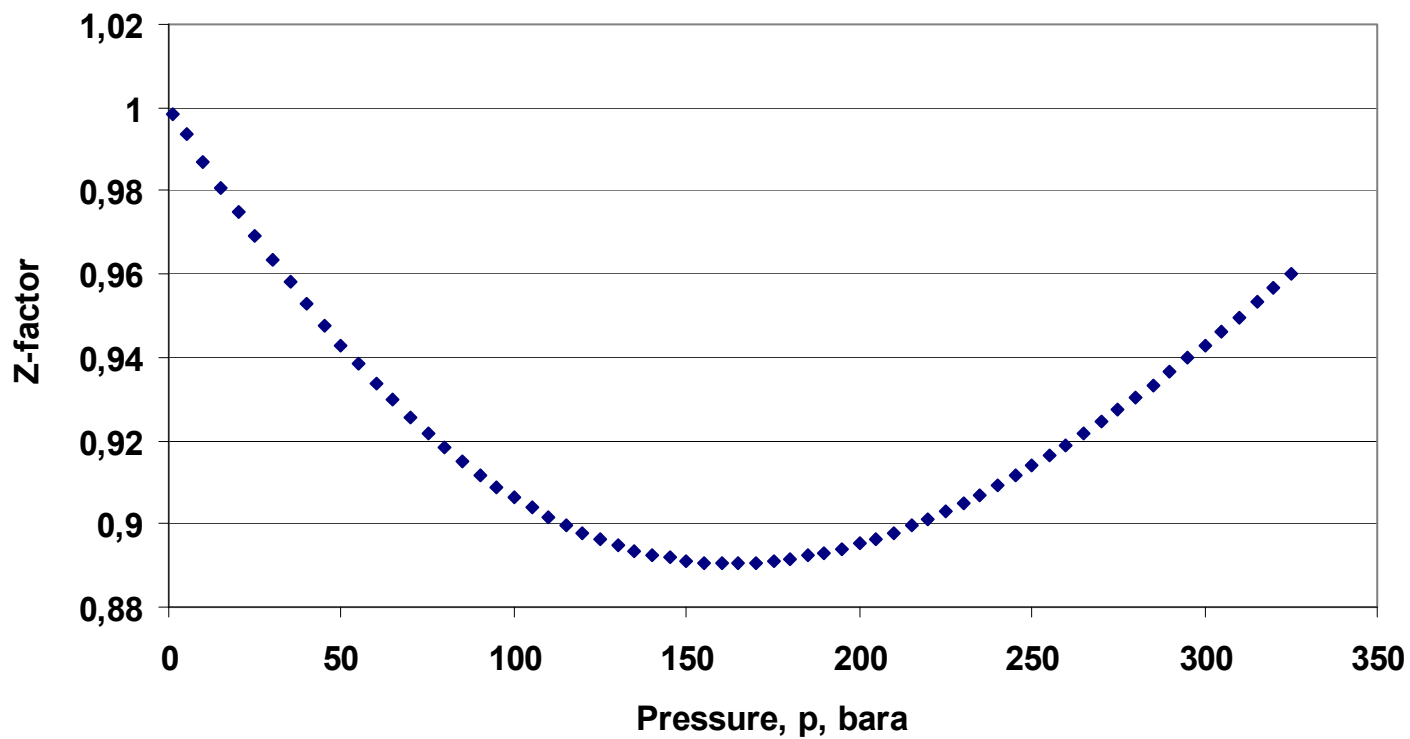
$G$  = Gas already produced ( $G_p$  in many texts)

Use FVF (symbol  $B$ ) for natural gas

$$(p/z) = (p_i/z_i) [1 - G/G_i]$$

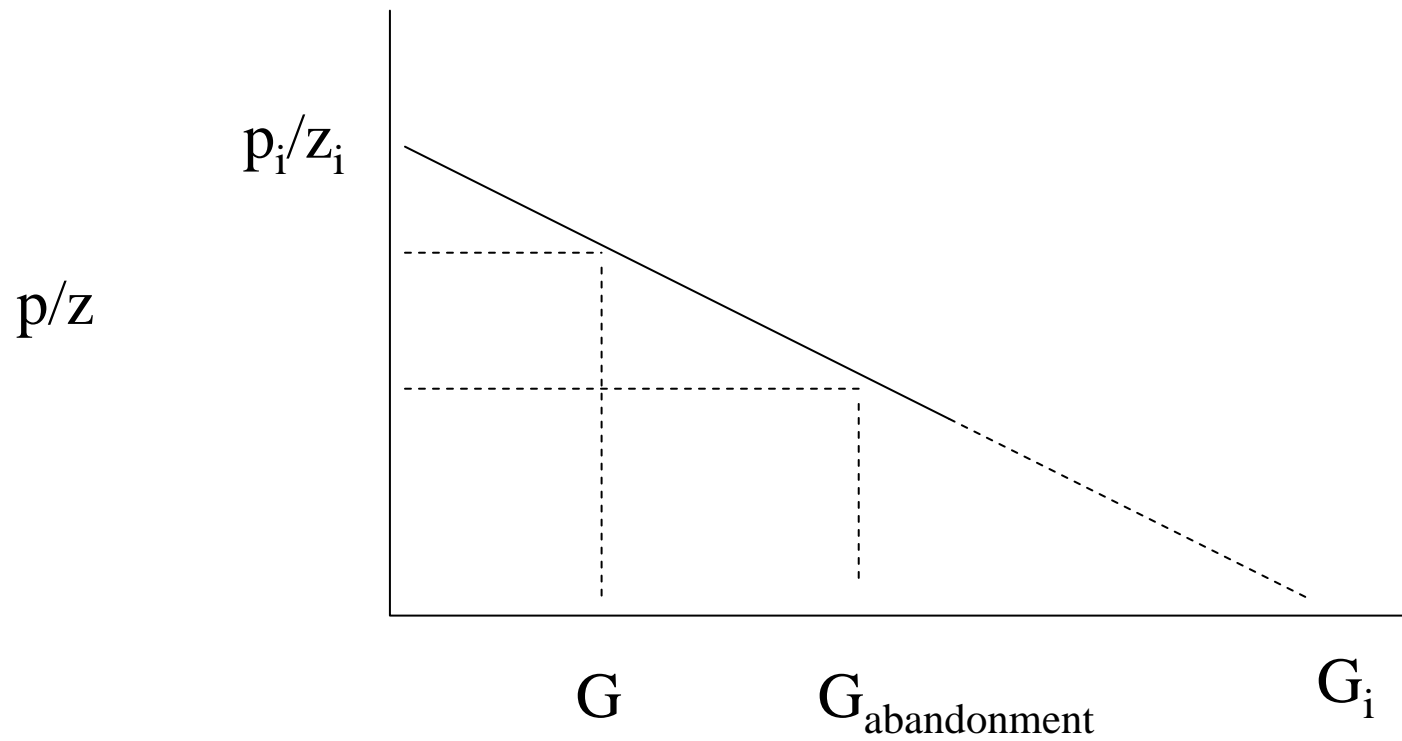


Z-factor Alpha Field Gas

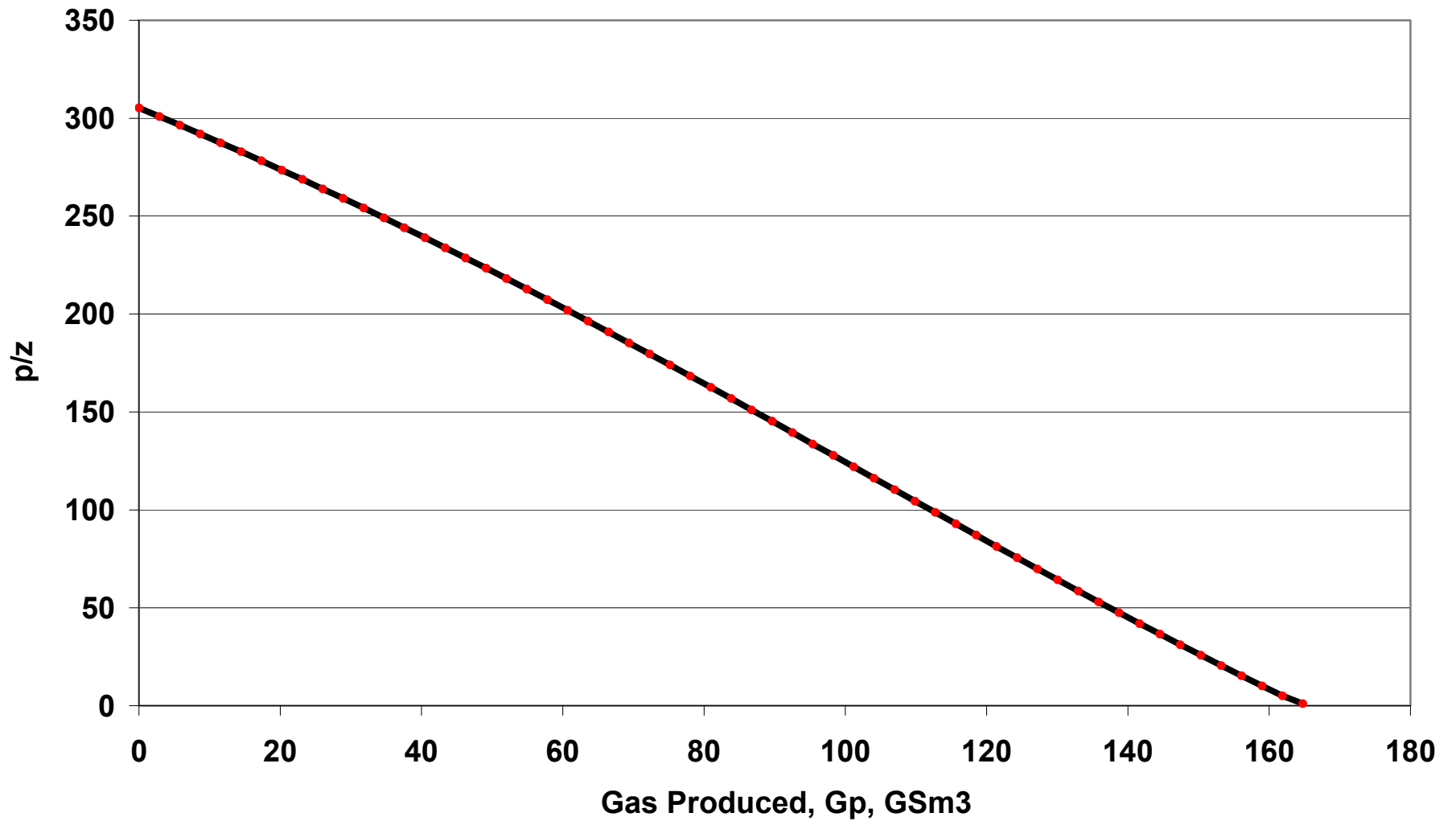


# Material Balance for Natural Gas Fields

p/z Method



### Material Balance Alpha Gas Field



# Flow Equations for Natural Gas in Reservoir

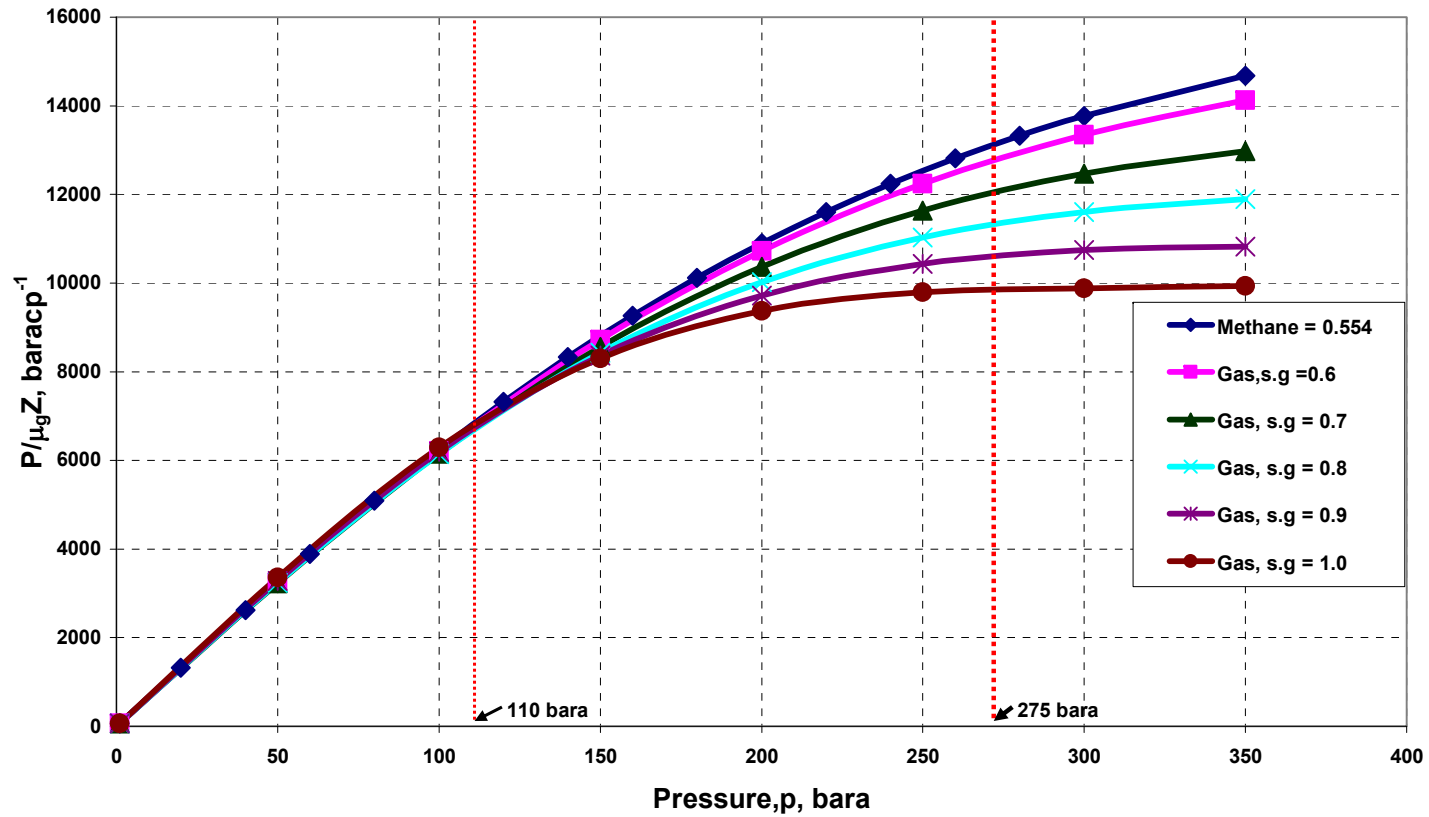
## Effect of Pressure

- In flow equations for low-pressure gas, pressure-squared is used,  $p_R^2 - p_w^2$ .
- When the pressure is intermediate, the so called pseudopressure  $m(p)$  is traditionally used (from numerical integration). Same as pressure function.
- At high-pressure, the gas behaves similar to liquid and the pressure drop is expressed by simple difference,  $p_R - p_w$ , which is the same as for conventional oil.
- What is low-pressure, intermediate pressure and high-pressure depends on the gas composition through the pressure function  $F(p) = \{p/(\mu z)\}$

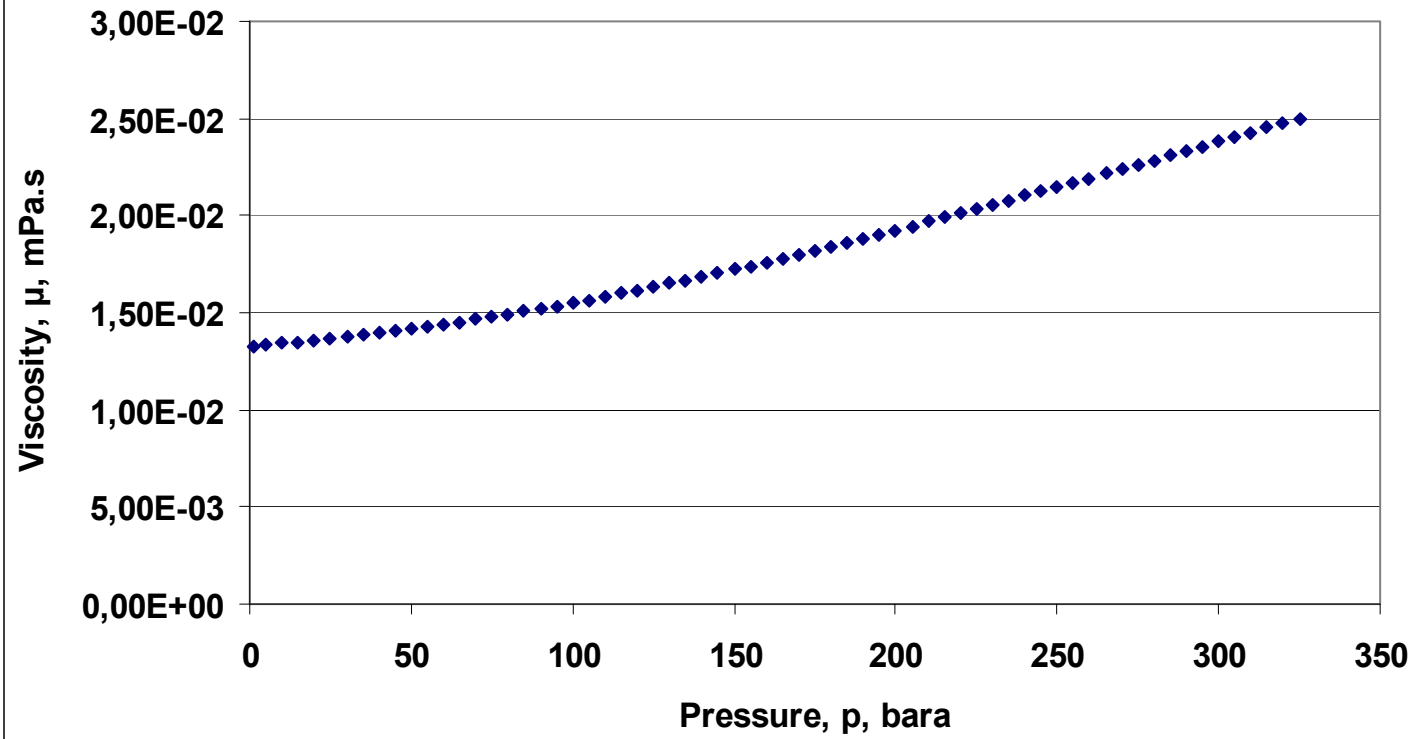
# PSS Rate Equation for Gas

$$q_{s.c.} = \frac{2\pi kh}{\left[ \ln\left(\frac{r_e}{r_w}\right) - \frac{3}{4} + s \right]} \left( \frac{T_{s.c.}}{T} \right) \left( \frac{1}{p_{s.c.}} \right) \int_{p_{wf}}^{p_R} \left( \frac{p}{\mu_g z} \right) dp$$

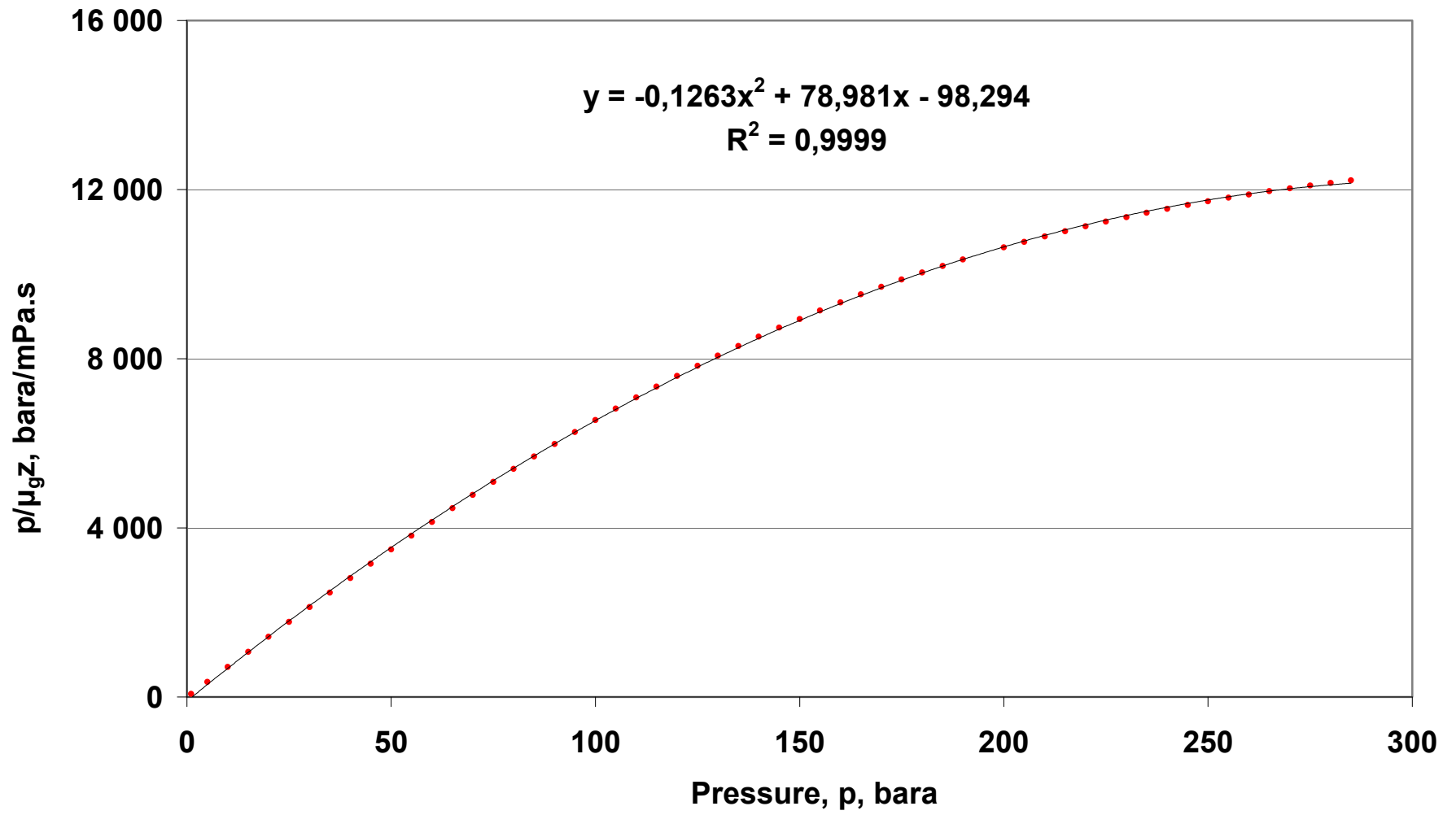
# Pseudopressure and Specific Gravity



### Viscosity



### Pseudo Pressure Alpha Field Gas





# High-Pressure Gas and Conventional Oil

$$q_{s.c.} = \frac{2\pi kh}{\left[ \ln\left(\frac{r_e}{r_w}\right) - \frac{3}{4} + s \right]} \left( \frac{T_{s.c.}}{T} \right) \left( \frac{1}{p_{s.c.}} \right) (p_R - p_{wf})$$

$$q = PI(p_R - p_{wf})$$

PI = Productivity Index

| <b>Well data ++</b>  |         |                     |
|--|---------|---------------------|
| Length of well, L  | 2600    | m                   |
| Wellhead pressure, p <sub>wf</sub> , (assume 80% of p <sub>R</sub> )   | 228     | bara                |
| Wellhead temperature, T <sub>wh</sub> (assumes 80% of T <sub>R</sub> ) | 70,4    | °C                  |
| Wellbore radius  | 0,1     | m                   |
| Tubing diameter  | 0,15    | m                   |
| Number of wells  | 6       |                     |
| Gas density at standard conditions, R <sub>ho</sub>                    | 0,74    | kg/S m <sup>3</sup> |
| Air density at standard conditions, R <sub>ho</sub>                    | 1,23    | kg/S m <sup>3</sup> |
| z- factor at standard conditions (ideal gas)                           | 1       |                     |
| Temperature at standard conditions, T <sub>sc</sub>                    | 15,56   | °C                  |
| Pressure at standard conditions  | 1,01325 | bara                |
| Life time of reservoir   | 20      | years               |
| Molecular weight of air, M <sub>air</sub>                              | 28,97   | kg/kmol             |

# Pressure Drop in Gas Wells

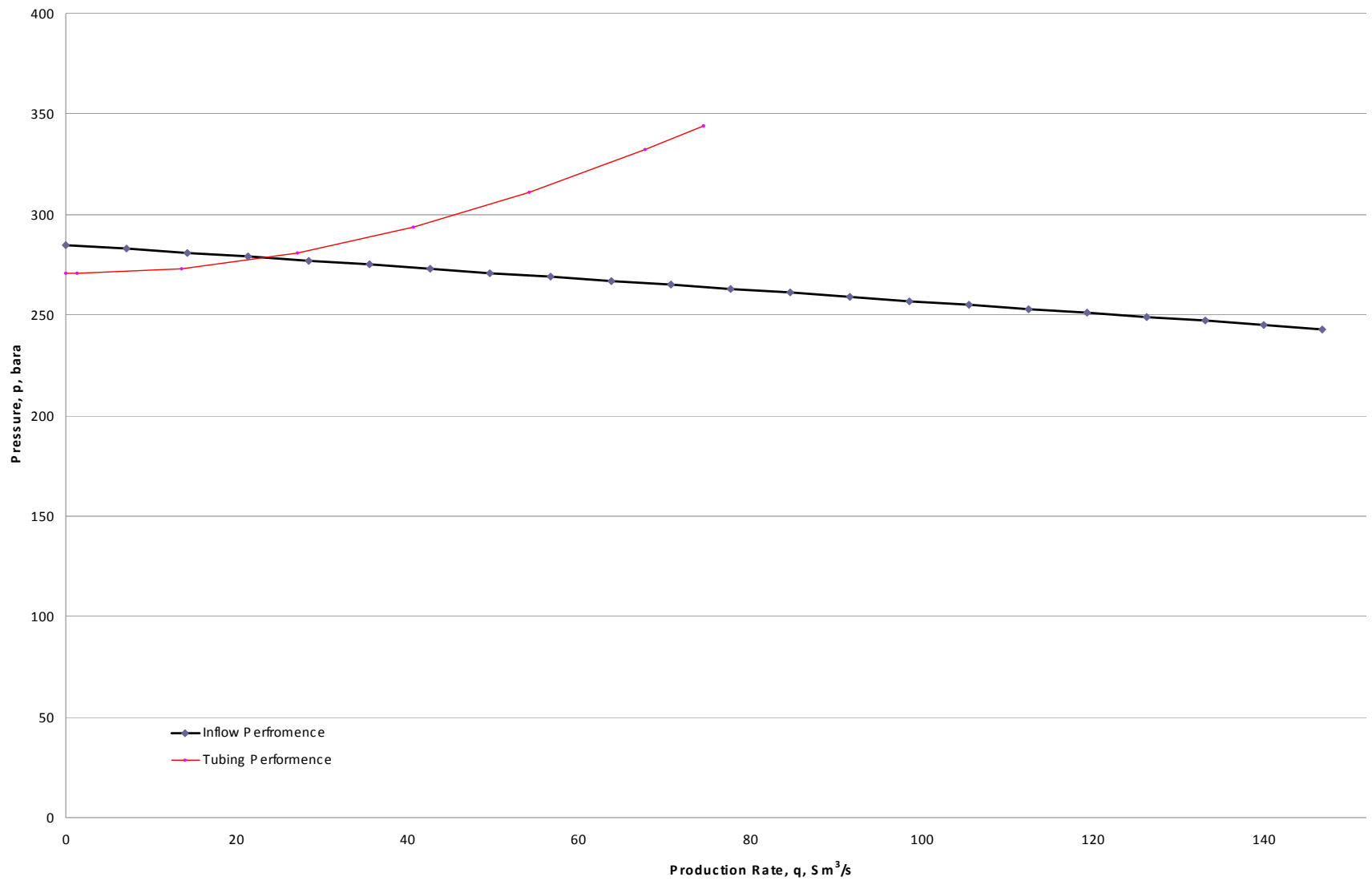
## Frictional and Hydrostatic

$$\Delta p = \Delta p_g + \Delta p_a + \Delta p_f$$

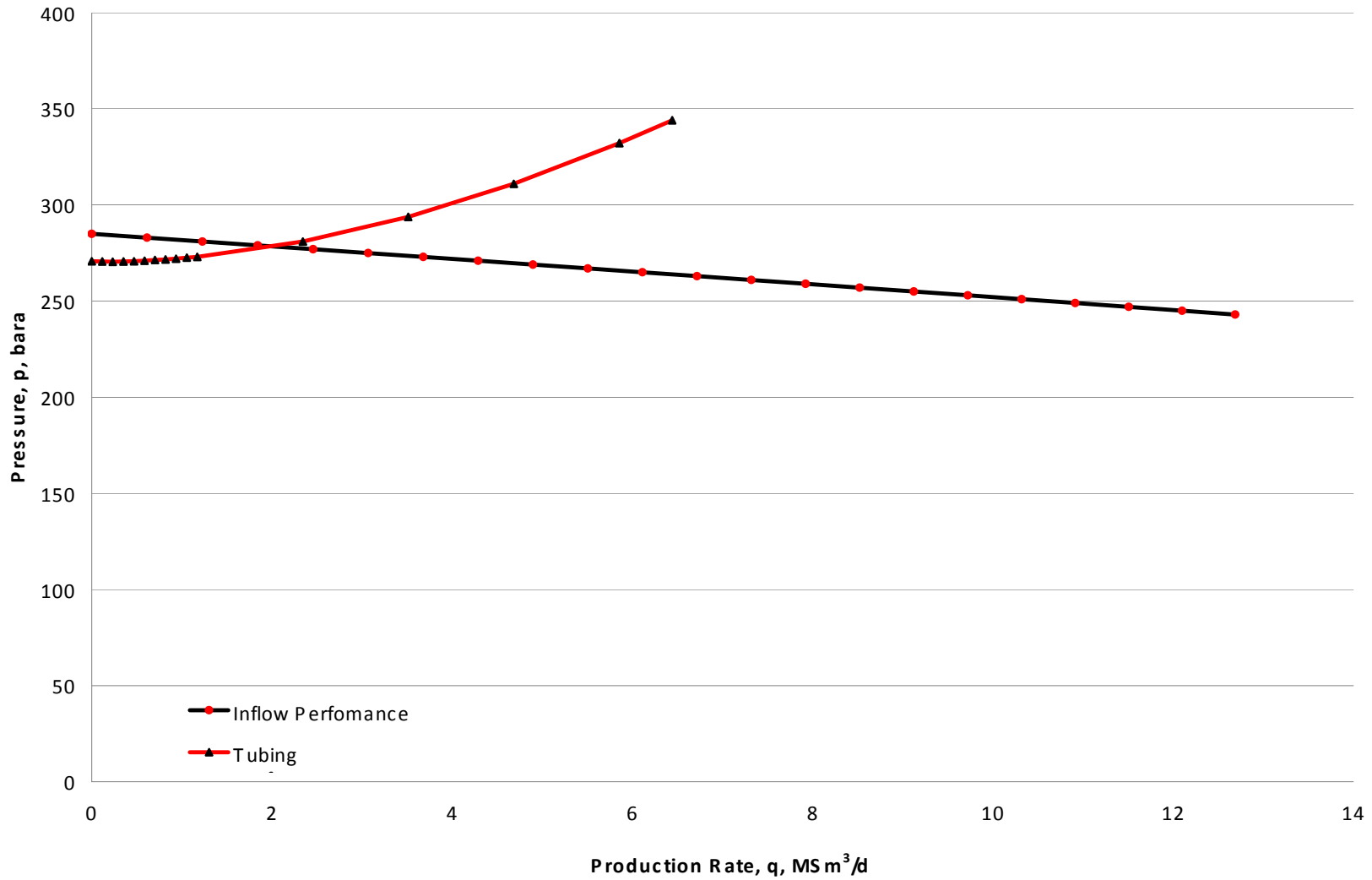
$$\frac{dA^2 M}{fm^2 zRT} (p_2^2 - p_1^2) - \frac{d}{f} \ln \left( \frac{p_2^2}{p_1^2} \right) + L = 0$$

$$p_2 = p_1 \exp \left[ - \left( \frac{M}{zRT} \right) (g \sin \alpha) \Delta L \right]$$

### Inflow Performance and Tubing Performance Alpha Wells



## Inflow Performance and Tubing Performance



# Summary

- Concept of deliverability can be used to estimate the production expected from a gas field from start-up to abandonment.
- The data presented for the Alpha field, the Alpha wells and the Alpha gas, is typical for a high-quality offshore resource.
- PSS rate equation using the general pressure function can be used for all inflow conditions.
- Established analytical equations for pressure drop in pipes can be used to calculate the outflow performance. (The presented outflow results were however obtained from Hysys calculations.)
- Inflow from high-pressure gas reservoirs (HPHT reservoirs, e.g. Kristin) behave similar to conventional oil reservoirs such that PI can be used.

# Reële gassloven

$$pV = znRT$$

$$pv = zRT$$

$$z_{sc} \cong 1$$

$$V_{sc} = V \left( \frac{p}{p_{sc}} \right) \left( \frac{T_{sc}}{T} \right) \left( \frac{1}{z} \right)$$

$$q_{sc} = q \left( \frac{p}{p_{sc}} \right) \left( \frac{T_{sc}}{T} \right) \left( \frac{1}{z} \right)$$

# Tetthet og FVF

$$pV = znRT$$

$$M = \frac{\rho V}{n}$$

$$\rho = \frac{pM}{znRT}$$

$$B(\equiv FVF) = \frac{V}{V_{sc}} \left( \frac{m^3}{Sm^3} \right)$$

$$B = \left( \frac{T}{T_{sc}} \right) \left( \frac{p_{sc}}{p} \right) z$$

$$q = q_{sc} B$$